

A CASCADED SEMI-BLIND SOURCE SEPARATION METHOD FOR JOINT ACOUSTIC ECHO CANCELLATION, INTERFERENCE SUPPRESSION, AND NOISE REDUCTION

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ABSTRACT

Acoustic echo cancellation (AEC), interference suppression, and noise reduction play important roles in full-duplex communication. However, conventional systems that cascade adaptive filters and beamformers often experience a degradation in performance during doubletalk situations. To tackle this issue, this paper presents a multichannel semi-blind-source-separation (SBSS) method that combines the element-wise iterative source steering (EISS) AEC algorithm with a geometrically constrained independent vector analysis source extraction algorithm for full-duplex communications. Simulation results confirm the effectiveness of the proposed method.

Index Terms— Acoustic echo cancellation, interference suppression, noise reduction, semi-blind source separation

1. INTRODUCTION

Acoustic echo cancellation (AEC), interference suppression, and noise reduction are fundamental tasks in full-duplex communications [1–3]. Consequently, numerous methods have been proposed over the past few decades to address these tasks either individually or jointly [4–10]. Among these, the adaptive filter followed by a post-beamformer has emerged as the most widely used approach [9]. However, in doubletalk scenarios where both far-end and near-end signals are active, the performance of such methods often degrades dramatically.

One way to enhance performance is by employing semi-blind source separation (SBSS) AEC algorithms [11–16]. While these algorithms are effective in handling doubletalk scenarios compared to traditional adaptive AEC algorithms, they are generally ineffective in dealing with near-end interference and noise. To address this issue, an offline joint AEC and source extraction algorithm based on independent vector analysis (IVA) was developed [17]. This algorithm shows promising performance when the near-end interference is relatively stationary compared to the target signal. However, in cases where the interference is non-stationary, there is a

risk of extracting the interference instead of the target signal, known as permutation ambiguity [18].

In certain applications, the location of the target signal can be determined by a camera or estimated based on the observation signals. As shown in [19–23], such spatial prior information can be used to greatly enhance separation performance and address the permutation problem. With this in mind, this paper introduces a multichannel SBSS method, which consists of two stages. The first stage employs EISS to eliminate echo effects. Subsequently, we extend our previous geometrically constrained IVA (GC-IVA) approach [22] to handle an overdetermined situation for jointly suppressing interference and reducing noise. We henceforth refer to the proposed method as EISS-GCIVA. Simulations are conducted to validate the effectiveness of the proposed EISS-GCIVA system in doubletalk situations with non-stationary near-end interference and noise.

2. SIGNAL MODEL AND PROBLEM FORMULATION

We consider a full duplex communication scenario where an array of M microphones is used. The loudspeaker is relatively far from the array while the near-end target speaker and interference are close to the array. The m -th microphone signal can be denoted as

$$y_m(t) = h_m(t) \star x(t) + a_{s,m}(t) \star s(t) + \sum_{n=1}^N a_{e,m,n}(t) \star e_n(t) + v(t), \quad (1)$$

where \star denotes convolution operation, t is the time index, $h_m(t)$ is the room impulse response (RIR) from the loudspeaker to the m -th microphone, $x(t)$ is the far-end signal, $a_{s,m}(t)$ and $a_{e,m,n}(t)$ represent, respectively, the RIRs from target source and the n -th interference positions to the m -th microphone, $s(t)$, $e_n(t)$, $v(t)$ are the target signal, the n -th interference signal, and the stationary background noise, respectively. In this study, We consider only determined or over-determined situations, i.e., $M \geq 1 + N$. To make the deduced algorithms computationally efficient, a convolutive transfer function (CTF) model [24] is adopted, which expresses the signals given in (1) in the short-time-

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Fourier-transform (STFT) domain as

$$Y_{m,i,j} = \sum_{l=0}^{L-1} H_{m,i,j-l} X_{i,j} + A_{s,m,i,j} S_{i,j} + \sum_{n=1}^N A_{e,m,n,i,j} E_{n,i,j} + V_{i,j}, \quad (2)$$

where i, j are, respectively, the frequency-bin and time-frame indices, $Y_{m,i,j}$, $X_{i,j}$, $S_{i,j}$, $E_{n,i,j}$ and $V_{i,j}$ are, respectively, the STFTs of $y_m(t)$, $x(t)$, $s(t)$, $e_n(t)$ and $v(t)$, and $H_{i,j-l}$, $A_{s,m,i,j}$, $A_{e,m,n,i,j}$ represent, respectively, $h_m(t)$, $a_{s,m}(t)$ and $a_{e,m,n}(t)$ in the STFT domain. The noisy near-end signal is defined as

$$Z_{m,i,j} = A_{s,m,i,j} S_{i,j} + \sum_{n=1}^N A_{e,m,n,i,j} E_{n,i,j} + V_{i,j}. \quad (3)$$

Without loss of generality, let us choose the first microphone as reference, then in matrix/vector form, (3) can be rewritten as

$$\mathbf{z}_{i,j} = \mathbf{a}_{s,i,j} A_{s,1,i,j} S_{i,j} + \sum_{n=1}^N \mathbf{a}_{e,n,i,j} A_{e,1,n,i,j} E_{n,i,j} + \mathbf{v}_{i,j}, \quad (4)$$

where

$$\begin{aligned} \mathbf{z}_{i,j} &= [Z_{1,i,j} \quad Z_{2,i,j} \quad \dots \quad Z_{M,i,j}]^T, \\ \mathbf{v}_{i,j} &= [V_{1,i,j} \quad V_{2,i,j} \quad \dots \quad V_{M,i,j}]^T, \\ \mathbf{a}_{s,i,j} &= \begin{bmatrix} 1 & \frac{A_{s,2,i,j}}{A_{s,1,i,j}} & \dots & \frac{A_{s,M,i,j}}{A_{s,1,i,j}} \end{bmatrix}^T, \\ \mathbf{a}_{e,n,i,j} &= \begin{bmatrix} 1 & \frac{A_{e,2,n,i,j}}{A_{e,1,n,i,j}} & \dots & \frac{A_{e,M,n,i,j}}{A_{e,1,n,i,j}} \end{bmatrix}^T. \end{aligned} \quad (5)$$

With the above CTF model, the problem in this study is to recover $A_{s,1,i,j} S_{i,j}$ given the multichannel observations and the reference signal $\mathbf{X}_{i,j}$.

3. CASCADED SEMI-BLIND SOURCE SEPARATION

In this section, we introduce a cascaded semi-blind-source-separation method comprising two stages: the first stage aims to eliminate the echo signal $\mathbf{z}_{i,j}$, while the second stage focuses on further suppressing near-end interference and noise.

3.1. AEC

In the first stage, the echo components can be expressed as

$$\tilde{\mathbf{y}}_{m,i,j} = \tilde{\mathbf{H}}_{m,i,j} \tilde{\mathbf{z}}_{m,i,j}, \quad (6)$$

where

$$\tilde{\mathbf{y}}_{m,i,j} = [Y_{m,i,j} \quad X_{i,j} \quad \dots \quad X_{i,j-L+1}]^T, \quad (7)$$

$$\tilde{\mathbf{z}}_{m,i,j} = [Z_{m,i,j} \quad X_{i,j} \quad \dots \quad X_{i,j-L+1}]^T, \quad (8)$$

$$\tilde{\mathbf{H}}_{m,i,j} = \begin{bmatrix} 1 & \mathbf{h}_{m,i,j}^T \\ \mathbf{0}_{L \times 1} & \mathbf{I}_L \end{bmatrix}, \quad (9)$$

with

$$\mathbf{h}_{m,i,j} = [H_{m,i,j} \quad H_{m,i,j-1} \quad \dots \quad H_{m,i,j-L+1}]^T. \quad (10)$$

The inverse process to estimate $\tilde{\mathbf{z}}_{m,i,j}$ can be written as

$$\tilde{\mathbf{z}}_{m,i,j} = \mathbf{W}_{m,i,j}^{\text{AEC}} \tilde{\mathbf{y}}_{m,i,j}, \quad (11)$$

where

$$\mathbf{W}_{m,i,j}^{\text{AEC}} = \begin{bmatrix} 1 & -\mathbf{h}_{m,i,j}^T \\ \mathbf{0}_L & \mathbf{I}_L \end{bmatrix}. \quad (12)$$

let us define the near-end extraction filter

$$\mathbf{w}_{m,i,j}^{\text{AEC}} = [1 \quad -\mathbf{h}_{m,i,j}^T]^H. \quad (13)$$

The near-end signal at the m -th microphone can then be estimated as

$$Z_{m,i,j} = (\mathbf{w}_{m,i,j}^{\text{AEC}})^H \tilde{\mathbf{y}}_{m,i,j}. \quad (14)$$

We model the near-end signal with a generalized Gaussian distribution (GCD), i.e., $\mathcal{N}_{\text{GCD}}(\mathbf{z}_{m,j}, \gamma_z, \beta_z)$, which is widely used in the literature of acoustic signal processing [25],

$$p(\mathbf{z}_{m,j}) \propto \exp \left[- \left(\frac{\|\mathbf{z}_{m,j}\|_2}{\gamma_z} \right)^{\beta_z} \right], \quad (15)$$

where $\|\cdot\|_2$ denotes ℓ_2 norm, γ_z and β_z are two shape parameters, and

$$\mathbf{z}_{m,j} = [Z_{m,1,j} \quad Z_{m,2,j} \quad \dots \quad Z_{m,I,j}]^T \quad (16)$$

is a vector consisting of all frequency components of the near-end signal. To utilize the well known majorization-minimization (MM) method [26], we assume that $\gamma_z > 0$, $0 < \beta_z \leq 2$. Then, exploiting the mutual independence between the far- and near-end signals, one can write the following auxiliary function

$$\mathcal{L}_{m,j}^{\text{AEC},+} = \sum_{i=1}^I (\mathbf{w}_{m,i,j}^{\text{AEC}})^H \mathbf{Q}_{m,i,j}^{\text{AEC}} \mathbf{w}_{m,i,j}^{\text{AEC}}, \quad (17)$$

where

$$\begin{aligned} \mathbf{Q}_{m,i,j}^{\text{AEC}} &= \alpha^{\text{AEC}} \mathbf{Q}_{m,i,j-1}^{\text{AEC}} \\ &+ (1 - \alpha^{\text{AEC}}) \varphi(r_{z,m,j}) \tilde{\mathbf{y}}_{m,i,j} \tilde{\mathbf{y}}_{m,i,j}^H, \end{aligned} \quad (18)$$

and

$$\varphi(r_{z,m,j}) = (r_{z,m,j})^{\beta_z-2}, \quad (19)$$

$$r_{z,m,j} = \sqrt{\sum_{i=1}^I |(\mathbf{w}_{m,i,j}^{\text{AEC}})^H \tilde{\mathbf{y}}_{m,i,j}|^2}. \quad (20)$$

The element-wise source steering (EISS) is a computationally efficient algorithm to minimize (17). EISS update each element in $\mathbf{w}_{m,i,j}^{\text{AEC}}$ individually with following update rule

$$W_{m,i,j,k}^{\text{AEC}} \leftarrow W_{m,i,j-1,k}^{\text{AEC}} - U_{m,i,j,k}^{\text{AEC}}, \quad k = 2, \dots, L+1, \quad (21)$$

where $W_{m,i,j,k}^{\text{AEC}}$ is the m -th element of $\mathbf{w}_{m,i,j}^{\text{AEC}}$ and $U_{m,i,j,k}^{\text{AEC}}$ is known as the steering step size. Substituting (21) into (17), calculating the derivative with respect to $(U_{m,i,j,k}^{\text{AEC}})^*$ (* denotes conjugate) and forcing the result to 0, we obtain

$$U_{m,i,j,k}^{\text{AEC}} = 1 - \left[(\mathbf{w}_{m,i,j-1}^{\text{AEC}})^H \mathbf{Q}_{m,i,j}^{\text{AEC}} \mathbf{w}_{m,i,j-1}^{\text{AEC}} \right]^{-\frac{1}{2}}. \quad (22)$$

Applying EISS to each channel, we obtain the estimated $\mathbf{z}_{i,j}$.

3.2. Interference suppression and noise reduction

Now, we extend our previous work [22] to further suppress the near-end noise and interference after AEC. Similar with the overdetermined IVA (OverIVA) [26, 27], we assume that the rank of $E[\mathbf{v}_{i,j}\mathbf{v}_{i,j}^H]$ matrix is $M-1-N$. Then following demixing matrix is used to extract the target signal

$$\mathbf{W}_{i,j}^{\text{IVA}} = \begin{bmatrix} \widetilde{\mathbf{W}}_{i,j}^{\text{IVA}} \\ \overline{\mathbf{W}}_{i,j}^{\text{IVA}} \end{bmatrix}. \quad (23)$$

Since our goal is to separate the noise from the target and interference signals, we employ the specific structure of $\overline{\mathbf{W}}_{i,j}^{\text{IVA}}$, corresponding to the OverIVA in this study. Specifically, we use:

$$\overline{\mathbf{W}}_{i,j}^{\text{IVA}} = [\Phi_{i,j} - \mathbf{I}_{M-1-N}], \quad (24)$$

where $\Phi_{i,j}$ contains adjustable parameters. Without loss of generality, we choose the first row in $\widetilde{\mathbf{W}}_{i,j}^{\text{IVA}}$, i.e., $\widetilde{\mathbf{w}}_{1,i,j}^{\text{IVA}}$, as the target extraction filter. To incorporate spatial prior information about the target and interference signal, we assume that

$$p(\widetilde{\mathbf{w}}_{n',i,j}^{\text{IVA}}) \propto \exp\left(-\sum_{i=1}^I \lambda_{n',j} \|\widetilde{\mathbf{w}}_{n',i,j}^{\text{IVA}} - \mathbf{d}_{\hat{\theta},i}\|_2^2\right), \quad (25)$$

where $\lambda_{n',j}$ is the weighting parameter,

$$\mathbf{d}_{\hat{\theta},i} = [1 \quad e^{-j\omega_i\tau_{2,\hat{\theta}}} \quad \dots \quad e^{-j\omega_i\tau_{M,\hat{\theta}}}]^T \quad (26)$$

is a steering vector and ω_i is the angular frequency corresponding to i -th frequency bin and $n' = 1, 2, \dots, N+1$. The time difference of arrival of the signal incident from $\hat{\theta}$ between the m -th and first microphones is denoted as $\tau_{m,\hat{\theta}}$. To use the MM method, we model the target signal and interference with a GCD as well, i.e., $p(\mathbf{s}_j) = \mathcal{N}_{\text{GCD}}(\mathbf{s}_j, \gamma_1, \beta_1)$ and $p(\mathbf{e}_{n,j}) = \mathcal{N}_{\text{GCD}}(\mathbf{e}_{n,j}, \gamma_{n+1}, \beta_{n+1})$ where

$$\mathbf{s}_j = [S_{1,j} \quad S_{2,j} \quad \dots \quad S_{I,j}]^T, \quad (27)$$

$$\mathbf{e}_{n,j} = [E_{n,1,j} \quad E_{n,2,j} \quad \dots \quad E_{n,I,j}]^T. \quad (28)$$

By adopting the maximum *a posteriori* (MAP) and MM method [28], we can derive the following recursive cost function

$$\begin{aligned} \mathcal{L}_j^{\text{IVA}}(\widetilde{\mathbf{W}}_{i,j}^{\text{IVA}}) &= \sum_{n'=1}^{N+1} \left[(\widetilde{\mathbf{w}}_{n',i,j}^{\text{IVA}})^H \mathbf{Q}_{n',i,j}^{\text{IVA}} \widetilde{\mathbf{w}}_{n',i,j}^{\text{IVA}} \right. \\ &\quad \left. + \lambda_{n',j} \|\widetilde{\mathbf{w}}_{n',i,j}^{\text{IVA}} - \mathbf{d}_{\hat{\theta},i}\|_2^2 \right] - 2 \sum_{i=1}^I \log |\det \mathbf{W}_{i,j}^{\text{IVA}}|, \end{aligned} \quad (29)$$

where $(\widetilde{\mathbf{w}}_{n',i,j}^{\text{IVA}})^H$ is the n' -th row of $\widetilde{\mathbf{W}}_{i,j}^{\text{IVA}}$ and

$$\mathbf{Q}_{n',i,j}^{\text{IVA}} = \alpha^{\text{IVA}} \mathbf{Q}_{n',i,j-1}^{\text{IVA}} + (1 - \alpha^{\text{IVA}}) \varphi(r_{n',j}) \mathbf{z}_{i,j} \mathbf{z}_{i,j}^H, \quad (30)$$

with

$$\varphi(r_{n',j}) = (r_{n',j})^{\beta_{n'}-2}, \quad (31)$$

$$r_{n',j} = \sqrt{\sum_{i=1}^I \left| (\mathbf{w}_{n',i,j}^{\text{IVA}})^H \mathbf{z}_{i,j} \right|^2}. \quad (32)$$

3.2.1. Update of $\widetilde{\mathbf{W}}_{i,j}^{\text{IVA}}$

Now, we estimate the demixing matrix with the geometrically constrained iterative source steering (GC-ISS) update rules, which are

$$\widetilde{\mathbf{W}}_{i,j}^{\text{IVA}} = \widetilde{\mathbf{W}}_{i,j-1}^{\text{IVA}} - \mathbf{u}_{m,i,j}^{\text{IVA}} (\mathbf{w}_{m,i,j-1}^{\text{IVA}})^H, \quad (33)$$

where

$$\mathbf{u}_{m,i,j}^{\text{IVA}} = [U_{m,i,j,1}^{\text{IVA}} \quad U_{m,i,j,2}^{\text{IVA}} \quad \dots \quad U_{m,i,j,N+1}^{\text{IVA}}]^T. \quad (34)$$

For each pair of m and n' , if $n' \neq m$, the optimal estimate of $U_{m,i,j,n'}^{\text{IVA}}$ is

$$\hat{U}_{m,i,j,n'}^{\text{IVA}} = \frac{G_{m,i,j,n'} + \lambda_{n',j} \tilde{\mathbf{d}}_{\hat{\theta},i}^H \mathbf{w}_{m,i,j-1}^{\text{IVA}}}{\tilde{G}_{m,i,j,n'} + \lambda_{n',j} (\mathbf{w}_{m,i,j-1}^{\text{IVA}})^H \mathbf{w}_{m,i,j-1}^{\text{IVA}}}, \quad (35)$$

where

$$G_{m,i,j,n'} = (\mathbf{w}_{n',i,j-1}^{\text{IVA}})^H \mathbf{Q}_{n',i,j}^{\text{IVA}} \mathbf{w}_{m,i,j-1}^{\text{IVA}}, \quad (36)$$

$$\tilde{G}_{m,i,j,n'} = (\mathbf{w}_{m,i,j-1}^{\text{IVA}})^H \mathbf{Q}_{n',i,j}^{\text{IVA}} \mathbf{w}_{m,i,j-1}^{\text{IVA}}, \quad (37)$$

$$\tilde{\mathbf{d}}_{\hat{\theta},i} = (\mathbf{w}_{n',i,j-1}^{\text{IVA}}) - \mathbf{d}_{\hat{\theta},i}, \quad (38)$$

while if $n' = m$, $U_{m,i,j,n'}^{\text{IVA}}$ is given as

$$\hat{U}_{m,i,j,n'}^{\text{IVA}} = \begin{cases} 1 - \eta_{i,j} \frac{|\eta_{i,j}| + \sqrt{|\eta_{i,j}|^2 + 4\zeta_{i,j}}}{2\zeta_{i,j}|\eta_{i,j}|}, & (\text{if } \eta_{i,j} \neq 0) \\ 1 - \frac{1}{\sqrt{\zeta_{i,j}}}, & (\text{else}) \end{cases} \quad (39)$$

where

$$\eta_{i,j} = \lambda_{m,j} \mathbf{d}_{\hat{\theta},i}^H \mathbf{w}_{m,i,j-1}^{\text{IVA}}, \quad (40)$$

$$\zeta_{i,j} = \tilde{G}_{m,i,j,m} + \lambda_{m,j} (\mathbf{w}_{m,i,j-1}^{\text{IVA}})^H \mathbf{w}_{m,i,j-1}^{\text{IVA}}. \quad (41)$$

3.2.2. Update of $\Phi_{i,j}$

After updating the first $N+1$ rows, the noise associated matrix is updated as

$$\Phi_{i,j} = \left[\mathbf{E}_2 \mathbf{C}_{i,j}^{\text{IVA}} (\widetilde{\mathbf{W}}_{i,j}^{\text{IVA}})^H \right] \left[\mathbf{E}_1 \mathbf{C}_{i,j}^{\text{IVA}} (\widetilde{\mathbf{W}}_{i,j}^{\text{IVA}})^H \right]^{-1}, \quad (42)$$

where

$$\mathbf{C}_{i,j}^{\text{IVA}} = \alpha^{\text{IVA}} \mathbf{C}_{i,j-1}^{\text{IVA}} + (1 - \alpha^{\text{IVA}}) \mathbf{z}_{i,j} \mathbf{z}_{i,j}^H, \quad (43)$$

$$\mathbf{E}_1 = [\mathbf{I}_N \quad \mathbf{0}_{N \times (M-N)}], \quad (44)$$

$$\mathbf{E}_2 = [\mathbf{0}_{(M-N) \times N} \quad \mathbf{I}_{M-N}]. \quad (45)$$

After updating the whole system, the near-end target signal will be extracted as

$$\hat{\mathbf{s}}_{i,j} = (\widetilde{\mathbf{w}}_{1,i,j}^{\text{IVA}})^H \mathbf{z}_{i,j}. \quad (46)$$

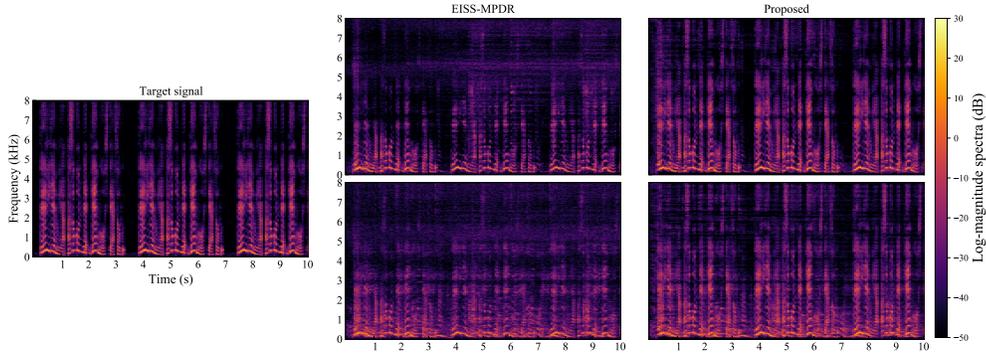


Fig. 1. Spectrograms of the extracted target signals. The first row corresponds to the target signals extracted in the first case. The second row corresponds to the extracted target signals in the second case.

4. SIMULATION

In this section, we evaluate the performance of the proposed EISS-GCIVA system. It is important to note that the multichannel state space method introduced in [29] cannot handle near-end interference and noise. Additionally, the joint blind source extraction and AEC algorithm discussed in [17] is offline. Therefore, to demonstrate the near-end noise reduction, interference suppression, and near-end signal preservation capabilities of the proposed method, we employ EISS with a post minimal power distortionless response (MPDR) beamformer as the baseline.

A room with dimensions of $8\text{ m} \times 8\text{ m} \times 3\text{ m}$ is simulated based on the image-source method [30]. For convenience, a Cartesian coordinate system is adopted, with the left-bottom corner of the room serving as the origin. A uniform linear microphone array consisting of 8 microphones, spaced 4 cm apart, is employed. The array is oriented parallel to the x -axis, with its center positioned at (4 m, 4 m, 1 m). A loudspeaker is positioned at (1 m, 4 m, 2.5 m). Additionally, a target speaker is located at (4.77 m, 4.64 m, 1.51 m), while an interference source is situated at (4 m, 5.2 m, 1.66 m). Three spatially distributed white Gaussian noise sources are randomly placed in the room, ensuring a minimum distance of 2 m from the microphone array.

We explore two scenarios. In the first case, we examine a less challenging setting where there is no interference present and the reverberation time t_{60} is set to 200 ms. For the second scenario, we consider a more challenging environment with t_{60} set to 400 ms, and the interference consists of a 10-second signal taken from the CHiME-3 Caf noise [31]. In both cases, the signal-to-echo ratio (SER) is maintained at 0 dB, the signal-to-noise ratio (SNR) at 20 dB, and both far- and near-end signals consist of 10-second-long speech signals from two female speakers. For the second scenario, the signal-to-interference ratio (SIR) is set to 10 dB. A 512-sample Von Hann window with 75% overlap is utilized, resulting in an algorithmic delay of 32 ms. The shape parameters β_z for the near-end mixture, β_1 for the target signal, and β_2 for interference are all set to 0.4. The forgetting factor α^{AEC} is set to 0.992, while α^{IVA} is set to 0.98. The initial

Table 1. Performance of the compared methods in the first case.

Systems	Case	oSINR	oSER	tERLE
EISS-MPDR	1	25.13	6.95	10.33
	2	20.79	4.69	8.26
EISS-GCIVA	1	33.19	9.74	10.30
	2	24.11	7.13	8.29

values of $\lambda_{n',0}$ are all set to 1 and decay during iterations according to $\lambda_{n',j} = \max(0.001, 0.8^j \times \lambda_{n',0})$. To mimic realistic conditions, biased direction estimates are provided. Specifically, the estimate of the target incidence angle is 20° when its actual angle is 40° , and the estimate of the interference incidence angle is 100° while it is actually 80° . We assess all the studied algorithms based on their output signal-to-interference-and-noise ratio (oSINR), output SER (oSER), and true return echo loss enhancement (tERLE) [11].

The results are presented in Table 1. It is seen that EISS-GCIVA achieves a higher oSINR compared to EISS-MPDR, indicating the superior near-end noise and interference suppression capabilities of the proposed method. Additionally, it is observed that EISS-MPDR demonstrates similar tERLE performance to EISS-GCIVA. This similarity arises because the echo is primarily estimated in the first stage. However, the oSER of EISS-GCIVA is significantly higher than that of EISS-MPDR. To illustrate this difference, we plot the spectrograms of the extracted target signals in Fig. 1. It is apparent that the target signal extracted by EISS-MPDR is distorted, whereas the quality of the target signal extracted by EISS-GCIVA is significantly superior, highlighting the effectiveness of the proposed method in preserving the target signal.

5. CONCLUSION

Effective joint acoustic echo cancellation and interference and noise suppression play a critical role in full-duplex communications. In this study, we introduced a cascaded semi-blind source separation method designed to eliminate echo while simultaneously suppressing near-end interference and noise in double-talk scenarios with minimal algorithmic delay. Simulation results confirmed the effectiveness of the proposed method.

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